

## Solving the Cam Compression Spring Problem

1. Investigate the loading and determine a max allowable shear stress

$$P_{max} = 600N, P_{min} = 300N$$

$$P_{mean} = 0.5 (P_{max} + P_{min}) = 0.5(900) = 450N$$

$$P_{alt} = 0.5 (P_{max} - P_{min}) = 0.5(300) = 150N$$

$$\text{Ratio of } P_{mean}/P_{alt} = 450/150 = 3$$

For a shot peened steel spring, fatigue endurance strength,  $S_{se} = 465MPa$

We don't know the wire diameter to determine  $S_{ut}$ , so we will pick a mid-range value to start with and adjust it later. It looks like a value of 1500MPa is midrange.

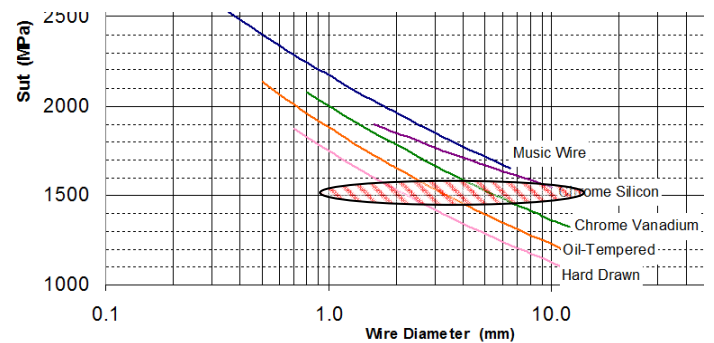
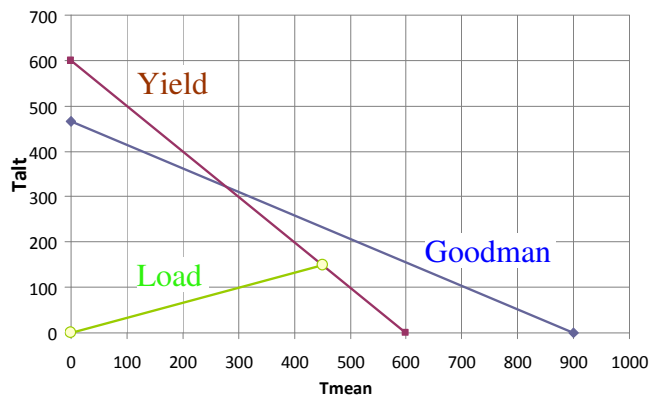
Then

$$\text{Shear Ultimate, } S_{su} = 0.6 S_{ut} = 900MPa$$

and

$$\text{Shear Yield, } S_{sy} = 0.4 S_{ut} = 600MPa$$

Now we can draw a Goodman diagram with a load line where  $\tau_{mean} = 3 \tau_{alt}$ :



We can see that the Yield Line actually limits the max shear stress. The intersection of the Load Line and the Yield Line gives

$$\frac{1}{FOS} = \frac{\tau_{alt}}{S_{sy}} + \frac{\tau_{mean}}{S_{su}} \text{ and because}$$

$$FOS = 1 \text{ and } \tau_{mean} = 3 \tau_{alt}$$

$$1 = \frac{\tau_{alt}}{600} + \frac{3\tau_{alt}}{600} = \frac{4\tau_{alt}}{600} = \frac{\tau_{alt}}{150}, \text{ or}$$

$$\tau_{alt} = 150MPa$$

2. Next, we see that the spring rate,  $k = \Delta P/\Delta X = (600-300)/25 = 300/25 = 12 N/mm$ .

We pick a midrange value for spring constant  $C = D/d$  of 8, and because this is cyclic loading we use the Bergstrasser factor

$$K_b = \frac{4C + 2}{4C - 3} = \frac{32 + 2}{32 - 3} = \frac{34}{29} = 1.172$$

Then we can write the equation for Shear Stress - I'll use alternating force and stress, but I could also have used means, maxes, or mins.

$$\tau_{alt} = \frac{8DK_b P_{alt}}{\pi d^3} = \frac{8CK_b P_{alt}}{\pi d^2} \text{ or } d^2 = \frac{8CK_b P_{alt}}{\pi \tau_{alt}} = \frac{(8)(8)(1.172)(150N)}{\pi(150MPa)} = 23.875 mm^2$$

$$\text{so } \boxed{d = 4.886mm}$$

Now that we know  $d$ , we can go back and calculate  $S_{ut}$ , but it turns out it is  $\sim 1540MPa$ .

Now we can calculate the mean diameter  $D = Cd = (8)(4.886) = 39.1\text{mm}$

3. Next, we can solve the spring rate equation to get  $N_a$ :

$$k = \frac{Gd}{8C^3 N_a (1 + 0.5/C^2)}$$
 and solve that for

$$N_a = \frac{Gd}{8kC^3 (1 + 0.5/C^2)} = \frac{(79,300\text{MPa})(4.886)}{(8)(12)(8)^3 (1 + 0.5/64)} = \frac{387,459.8}{(49,152)(1.0078)} = 7.82$$

and being Squared and Ground means that  $N_{tot} = N_a + 2 = 9.82$  turns,  
and that  $L_{solid} = dN_{tot} = (4.886)(9.82) = 48.0\text{mm}$

4. Add 10% of  $L_{solid}$  for margin, and add to that the max spring deflection at  $600\text{N} = 600/12 = 50\text{mm}$ :

$$L_{free} = (1.1)(48) + 50 = 52.8 + 50 = 102.8\text{mm}$$

5. For buckling, calculate

$$L_{free}/D = 102.8/39.1 = 2.63$$
 and

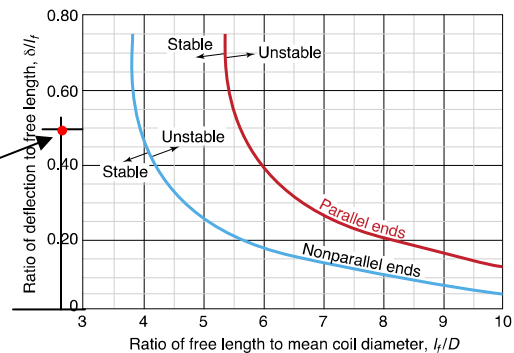
$$\Delta X_{max}/L_{free} = 50/102.8 = 0.49$$

so we are definitely stable, per Fig. 17.8

6. Finally, for steel springs, the natural frequency is

$$f = \frac{353,000d}{N_{tot} D^2} = \frac{(353,000)(4.886)}{(9.82)(39.09)^2} = 114.9\text{ Hz}$$

The cam is running at  $650\text{ RPM} = 650/60 = 10.8\text{Hz}$ , so that should not be problem.



## ASSIGNMENT

1. Design your own spring for this application. You can use the Spring Design spreadsheet calculator on the ME311 web page.
2. Find a spring from an online catalog (any manufacturer) that you could buy for this application. You may need to tweak some dimensions from those calculated.