

Bending and Torsional Stress

HW 3.1

| | | |
|---|---------|-----------|
| R | 6 in | Short Arm |
| L | 15 in | Long Arm |
| D | 0.75 in | Diameter |
| F | 100 lb | Force |

| | |
|-----|-----------|
| Sut | 76000 psi |
| Sy | 42000 psi |

| | | |
|----------------|------------------------|--------------------------|
| I | 0.0155 in ⁴ | =PI()*D ⁴ /64 |
| J | 0.0311 in ⁴ | =PI()*D ⁴ /32 |
| C ₋ | 0.375 in | =D/2 |
| A | 0.442 in ² | =PI()*D ² /4 |
| Torsion Moment | 600 in lb | =F*R ₋ |
| | 1500 in lb | =F*L |

| | | |
|-----------------|---------------|----------------------|
| MaxBending | 36,216.59 psi | =M*C ₋ /I |
| MaxTorsion | 7,243.32 psi | =T*(D/2)/J |
| AvgShear | 226.4 psi | =F/A |
| TransverseShear | 301.8 psi | =4*F/(3*A) |

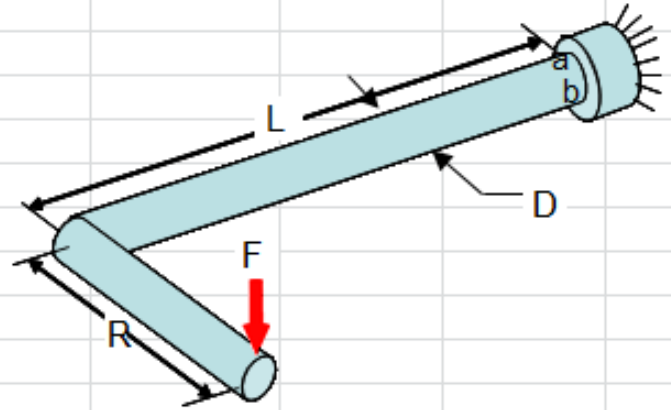
At "a":

| | | |
|--------|---------------|------------|
| SigmaX | 36,216.59 psi | MaxBending |
| SigmaY | 0 psi | |
| TauXY | 7,243.32 psi | MaxTorsion |

At "b":

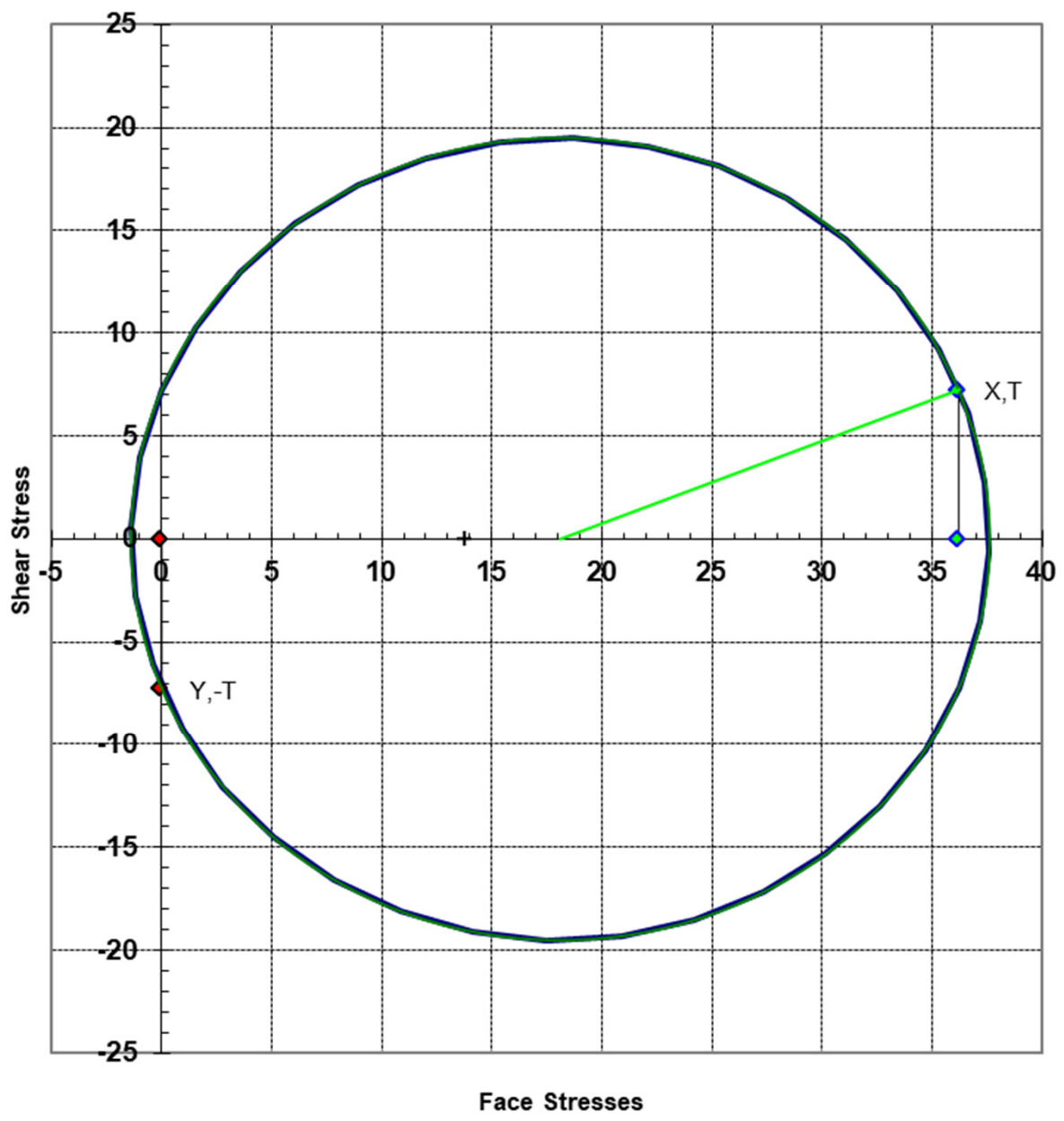
| | | |
|--------|-------------|-------------------------------|
| SigmaX | 0 psi | |
| SigmaY | 0 psi | |
| TauXY | 7545.12 psi | MaxTorsion + Transverse Shear |

At "b", Sigma1 = Sigma2 = TauXY = 7545 psi



Mohr's Circle for "a"

For Xstress = 36.2, Ystress = 0.0, XYShear = 7.2, Angle = 10.90,
Stress1 = 37.61, Stress2 = 0.00, Stress3 = -1.39, ShearMax = 19.50

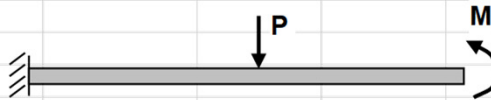


Deflection of the Beam Tip at F

| | | | | | |
|----------------------|------------|--------------------|-----------------------------|--|--|
| E | 10,100,000 | lb/in ² | | | |
| Poisson | 0.33 | | | | |
| G | 3,796,992 | lb/in ² | =E/(2*(1+Poisson)) | $G = \frac{E}{2(1 + \nu)}$ | |
| Bending of Short Arm | | | | | |
| Ybs | 0.0459 | in | =F*R_ ³ /(3*E*I) | $y = \frac{Fl^3}{3EI}$ | |
| Bending of Long Arm | | | | | |
| Ybl | 0.7172 | in | =F*L ³ /(3*E*I) | $y = \frac{Fl^3}{3EI}$ | |
| Twist of Long Arm | | | | | |
| ThetaL | 0.0763 | Rad | =T*L/(J*G) | $\theta = \frac{Tl}{JG}, \quad y = \theta R$ | |
| | 4.37 | ° | =ThetaL*180/PI() | | |
| Yts | 0.4578 | in | =R_*ThetaL | | |
| Ytotal | 1.221 | in | =Ybs+Ybl+Yts | | |

HW 3.2

| | | | |
|---------|---|------|-----|
| Base | b | 0.04 | m |
| Height | h | 0.1 | m |
| Length | L | 2 | m |
| Modulus | E | 207 | GPa |



| | | | | |
|--------------|---|------------|----------------|-----------------------|
| MomOfInertia | I | 3.3333E-06 | m ⁴ | =b*h ³ /12 |
|--------------|---|------------|----------------|-----------------------|

| | | | |
|----------|---|------|---|
| Load | P | 4000 | N |
| Location | a | 1.2 | m |

| | | | |
|--------|---|------|----|
| Moment | M | 2500 | Nm |
|--------|---|------|----|

We use Superposition to determine the deflections first from the Force and then from the Moment and then we add them together at P and at the Tip.

$$y = \frac{Px^2}{6EI}(3a - x) \text{ for } 0 < x < a$$

$$y = \frac{Pa^2}{6EI}(3x - a) \text{ for } a < x < l$$

From Hamrock Appendix D.2

Deflections due to Force P

| | | | | |
|----------|-----------|----|--|--|
| At P | | | | |
| XP | 1.2 | m | =a | |
| YP-Force | -0.003339 | m | =IF(XP<a,P*XP^2/(6*E*10^9*I)*(XP-3*a),P*a^2/(6*E*10^9*I)*(a-3*XP)) | |
| | -3.339 | mm | | |

| | | | | |
|------------|-----------|----|--|--|
| At Tip | | | | |
| Xtip | 2 | m | =L | |
| Ytip-Force | -0.006678 | m | =IF(Xtip<a,P*Xtip^2/(6*E*10^9*I)*(Xtip-3*a),P*a^2/(6*E*10^9*I)*(a-3*Xtip)) | |
| | -6.678 | mm | | |

Deflections due to Moment M

| | | | | |
|-----------|----------|----|----------------------|--|
| At P | | | | |
| XP | 1.2 | m | =a | |
| YP-Moment | 0.002609 | m | =M*XP^2/(2*E*10^9*I) | |
| | 2.609 | mm | | |

From Hamrock Appendix D.4

| | | | | |
|-------------|----------|----|------------------------|--|
| At Tip | | | | |
| Xtip | 2 | m | =L | |
| Ytip-Moment | 0.007246 | m | =M*Xtip^2/(2*E*10^9*I) | |
| | 7.246 | mm | | |

$$y = \frac{Mx^2}{2EI}$$

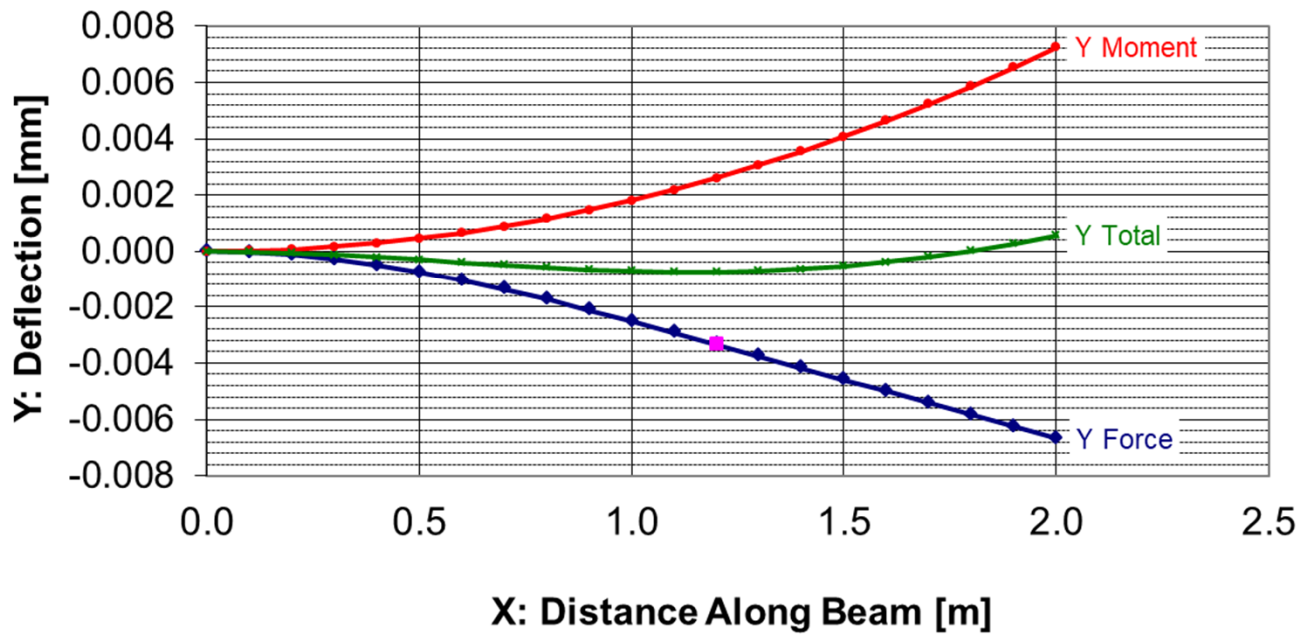
| X At P | y Force | y Moment | y Total |
|--------|---------|----------|---------|
| 1.2 | -3.339 | 2.609 | -0.730 |

| X At Tip | y Force | y Moment | y Total |
|----------|---------|----------|---------|
| 2 | -6.678 | 7.246 | 0.568 |

For Zero deflection at P, deflection from Moment must equal deflection from Force P, which is -3.339 mm. So we just proportion the Moment by the ratio of the deflections to reduce the deflection. In other words, if 2,500 Nm caused 2.609mm deflection, how much moment causes 3.339mm deflection? Deflection is directly proportional to force or moment, so we just proportion the Moment.

| | | |
|----------|---------|------------------------|
| M target | 3200 Nm | =M*YP_Force/-YP_Moment |
|----------|---------|------------------------|

Deflection [mm] Due to 4,000N Force & 2,500 Nm Moment



| X | Deflection (mm) | | |
|-----|-----------------|----------|---------|
| | Y Force | Y Moment | Y Total |
| 0.0 | 0.000 | 0.0000 | 0.000 |
| 0.1 | -0.034 | 0.0181 | -0.016 |
| 0.2 | -0.131 | 0.0725 | -0.059 |
| 0.3 | -0.287 | 0.1630 | -0.124 |
| 0.4 | -0.495 | 0.2899 | -0.205 |
| 0.5 | -0.749 | 0.4529 | -0.296 |
| 0.6 | -1.043 | 0.6522 | -0.391 |
| 0.7 | -1.373 | 0.8877 | -0.485 |
| 0.8 | -1.731 | 1.1594 | -0.572 |
| 0.9 | -2.113 | 1.4674 | -0.646 |
| 1.0 | -2.512 | 1.8116 | -0.700 |
| 1.1 | -2.923 | 2.1920 | -0.731 |
| 1.2 | -3.339 | 2.6087 | -0.730 |
| 1.3 | -3.757 | 3.0616 | -0.695 |
| 1.4 | -4.174 | 3.5507 | -0.623 |
| 1.5 | -4.591 | 4.0761 | -0.515 |
| 1.6 | -5.009 | 4.6377 | -0.371 |
| 1.7 | -5.426 | 5.2355 | -0.191 |
| 1.8 | -5.843 | 5.8696 | 0.026 |
| 1.9 | -6.261 | 6.5399 | 0.279 |
| 2.0 | -6.678 | 7.2464 | 0.568 |